

A simplified model of gear test rig is shown in Fig. 1. It consists of a driver and loader which permits rotation (Single degree of freedom system), the gear and pinion can translate in vertical (y_1 and y_2) and it can rotate about its axis (two degrees of freedom system) and the driver and loader are connected by connecting shafts which is mounted on bearings and foundations which permits translational motion in vertical (y_3 and y_4) thus a single degree of freedom system and the transducer is placed on a platform that permits translation in vertical (y_p) single degree of freedom system.

The governing equations of motion of the mathematical model of the gear system can be written as

$$I_d \ddot{\theta}_d + c_{t1}(\dot{\theta}_d - \dot{\theta}_1) + k_{t1}(\theta_d - \theta_1) = T_d \quad (1)$$

$$I_1 \ddot{\theta}_1 + c_{t1}(\dot{\theta}_1 - \dot{\theta}_d) + k_{t1}(\theta_1 - \theta_d) = -WR_1 \quad (2)$$

$$I_2 \ddot{\theta}_2 + c_{t2}(\dot{\theta}_2 - \dot{\theta}_l) + k_{t2}(\theta_2 - \theta_l) = WR_2 \quad (3)$$

$$I_l \ddot{\theta}_l + c_{t2}(\dot{\theta}_l - \dot{\theta}_2) + k_{t2}(\theta_l - \theta_2) = -T_l \quad (4)$$

$$m_1 \dot{y}_1 + c_1(\dot{y}_1 - \dot{y}_3) + k_1(y_1 - y_3) = W \quad (5)$$

$$m_2 \dot{y}_2 + c_2(\dot{y}_2 - \dot{y}_4) + k_2(y_2 - y_4) = -W \quad (6)$$

$$m_3 \ddot{y}_3 + c_{34}(\dot{y}_3 - \dot{y}_4) + k_{34}(y_3 - y_4) + c_1(\dot{y}_3 - \dot{y}_1) + k_1(y_3 - y_1) + c_p(\dot{y}_3 - \dot{y}_p) + k_p(y_3 - y_p) + c_3 \dot{y}_3 + k_3 y_3 = 0 \quad (7)$$

$$m_4 \ddot{y}_4 + c_{34}(\dot{y}_4 - \dot{y}_3) + k_{34}(y_4 - y_3) + c_2(\dot{y}_4 - \dot{y}_2) + k_4(y_4 - y_2) + c_4 \dot{y}_4 + k_4 y_4 = 0 \quad (8)$$

$$m_p \ddot{y}_p + c_p(\dot{y}_p - \dot{y}_3) + k_p(y_p - y_3) = 0 \quad (9)$$

where, W is the dynamic meshing force given by

$$W = k_m(\theta_1 R_1 - \theta_2 R_2 + y_2 - y_1) + c_m(\dot{\theta}_1 R_1 - \dot{\theta}_2 R_2 + \dot{y}_2 - \dot{y}_1) + c_m \dot{x}_E + k_m x_E \quad (10)$$

The equations of motion are solved in Matlab-Simulink environment using ODE-45 solver to find out the response. Gear fault like missing tooth is modeled for higher contact ratio gear system. The responses are computed for healthy and faulted condition in higher contact ratio gear system. The obtained vibration responses are analyzed in time domain and frequency domain. In both time as well as frequency domain, it is observed that there are peaks of higher magnitudes in faulted condition as compare to healthy condition and it is due to the impulsive dynamic forces induced in fault conditions.

References

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